

**Comparing Samples # 2; # 3 & # 4**

Both models I and II of blanket manufacturer B have a 3 ply wet-on-wet layer building and microscope inspection of the cross section of both samples show good reinforcement wetting and a virtually void-free structure. In model II a glue film was added between the compressive ply and the compressive sponge.

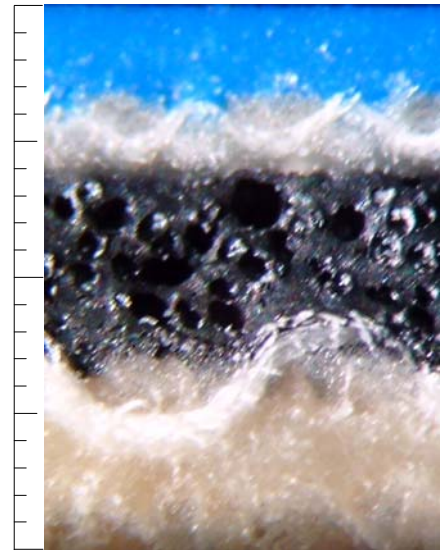
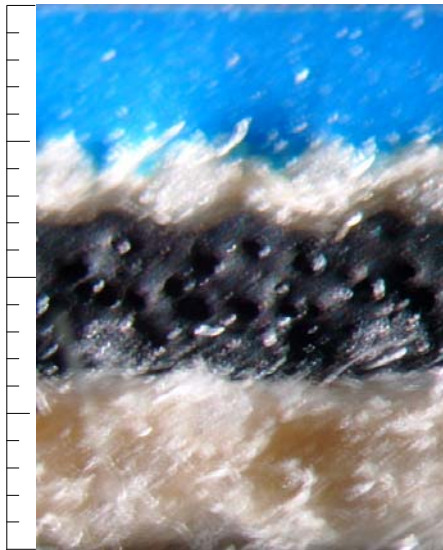
However samples 2; 3 and 4 show distinct properties worth consideration, as summarised:

Parameter	Sample #2	Sample #3	Sample #4
I <sub>1</sub> (1 <sup>st</sup> cycle Indentation)	165 µm	115 µm	179 µm
I <sub>5</sub> (5 <sup>th</sup> cycle Indentation)	136 µm	82 µm	142 µm
CL (Compression Loss)	17,9 %	28,8 %	20,6 %
HE (Hysteresis Energy)	0,26 Nmm	0,18 Nmm	0,70 Nmm
DC (Damping Capacity)	3,9 %	4,4 %	9,0 %

Samples 2 & 4 show a typical indentation value for sheetfed printing.

Samples 2 & 3 present low hysteresis losses.

Sample 3 shows high compression loss and insufficient indentation.



Photos of blanket samples with higher indentation show a thicker compressive sponge layer with more and larger holes.

Maybe low hysteresis losses (not so usual with traditional blanket models) should be linked to the wet-on-wet construction method.

An explanation for the comparatively higher hysteresis energy value measured on sample 4 would be a longer time interval between completion of the compressive layer and the interface glue film to the compressive ply spreading operation.

Note: Some test results of rubber composites with an almost pure spring-like behaviour - very low hysteresis - may fall outside the boundaries of present test scope. Test equipment carriage inversion points involve a relatively large inertia energy that may prevent even a gross assessment of blanket hysteresis and other energy related parameters, both at standard test speed or even at equipment lowest speed.